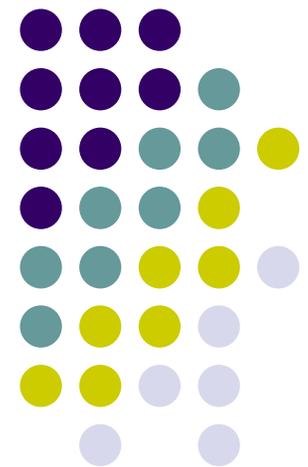


# ME751

## Advanced Computational Multibody Dynamics

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Section 9.2  
September 16, 2016



# Quote of the day



“I only believe in statistics that I doctored myself.”  
-- Sir Winston S. Churchill

# Before we get started...



- Last Time:
  - Changing the RF for representing a Geometric Vector
  - The concept of orientation matrix  $\mathbf{A}$
  - Angular velocity  $\omega$  of a rigid body
    - An attribute of a body, not of a reference frame attached to that body
    - Handy to express the time derivative of an orientation matrix:  $\dot{\mathbf{A}} = \tilde{\omega}\mathbf{A}$
  - Degree of freedom count, relative to 3D rotation of a rigid body
    - Given three direction cosines, you can find the other six to assemble  $\mathbf{A}$
- Today:
  - Hopping from RF to RF
  - Describing the orientation of a body using Euler Angles
  - Connection between the angular velocity and time derivatives of Euler Angles

# Next Assignment



- Due on September 23, 9:30 AM
- Assignment has two components
  - Component 1: read the proposal and provide feedback by Saturday evening
    - PDF of proposal to be emailed to you Friday by mid-day
    - Second version of the PDF will be emailed to you on Saturday at noon
      - Use either PDF version
      - Make comments and highlight things that don't make sense (instructions in follow-up email)
  - Component 2: the usual pen and paper stuff, to be emailed to you



[Short Detour:]

# Hopping from RF to RF

- The discussion framework:
  - Recall that when going from one L-RF<sub>2</sub> to a different L-RF<sub>1</sub>, there is a transformation matrix that multiplies the representation of a geometric vector in L-RF<sub>2</sub> to get the representation of the geometric vector in L-RF<sub>1</sub> :

$$\bar{s}_1 = \mathbf{A}_{12} \cdot \bar{s}_2$$

- Question: What happens if you want to go from L-RF<sub>3</sub> to L-RF<sub>2</sub> and then eventually to the representation in L-RF<sub>1</sub> ?
- Why bother?
  - This comes into play when dealing with Euler Angles



[End Detour:]

# Hopping from RF to RF

- Going from L-RF<sub>3</sub> to L-RF<sub>2</sub> to L-RF<sub>1</sub> :

$$\bar{\mathbf{s}}_2 = \mathbf{A}_{23} \cdot \bar{\mathbf{s}}_3 \quad \oplus \quad \bar{\mathbf{s}}_1 = \mathbf{A}_{12} \cdot \bar{\mathbf{s}}_2 \quad \Rightarrow \quad \bar{\mathbf{s}}_1 = \mathbf{A}_{12} \mathbf{A}_{23} \cdot \bar{\mathbf{s}}_3$$

- The basic idea: you keep multiplying rotation matrices like above to hope from RF to RF until you arrive to your final destination

- Question [relevant in one week]: How do we compute  $\mathbf{A}_{ij}$  if we have  $\mathbf{A}_i$  and  $\mathbf{A}_j$ ?
  - $\mathbf{A}_i$  : hopping from L-RF<sub>i</sub> to G-RF
  - $\mathbf{A}_{ij}$  : hopping from L-RF<sub>j</sub> to L-RF<sub>i</sub>
  - Keep in mind the invariant here; i.e., the GV  $\bar{\mathbf{s}}$  :

$$\left. \begin{array}{l} \mathbf{s} = \mathbf{A}_i \bar{\mathbf{s}}_i \\ \mathbf{s} = \mathbf{A}_j \bar{\mathbf{s}}_j \end{array} \right\} \Rightarrow \mathbf{A}_i \bar{\mathbf{s}}_i = \mathbf{A}_j \bar{\mathbf{s}}_j \Rightarrow \bar{\mathbf{s}}_i = \mathbf{A}_i^T \mathbf{A}_j \bar{\mathbf{s}}_j \Rightarrow \boxed{\mathbf{A}_{ij} = \mathbf{A}_i^T \mathbf{A}_j}$$

# A Matter of Notation



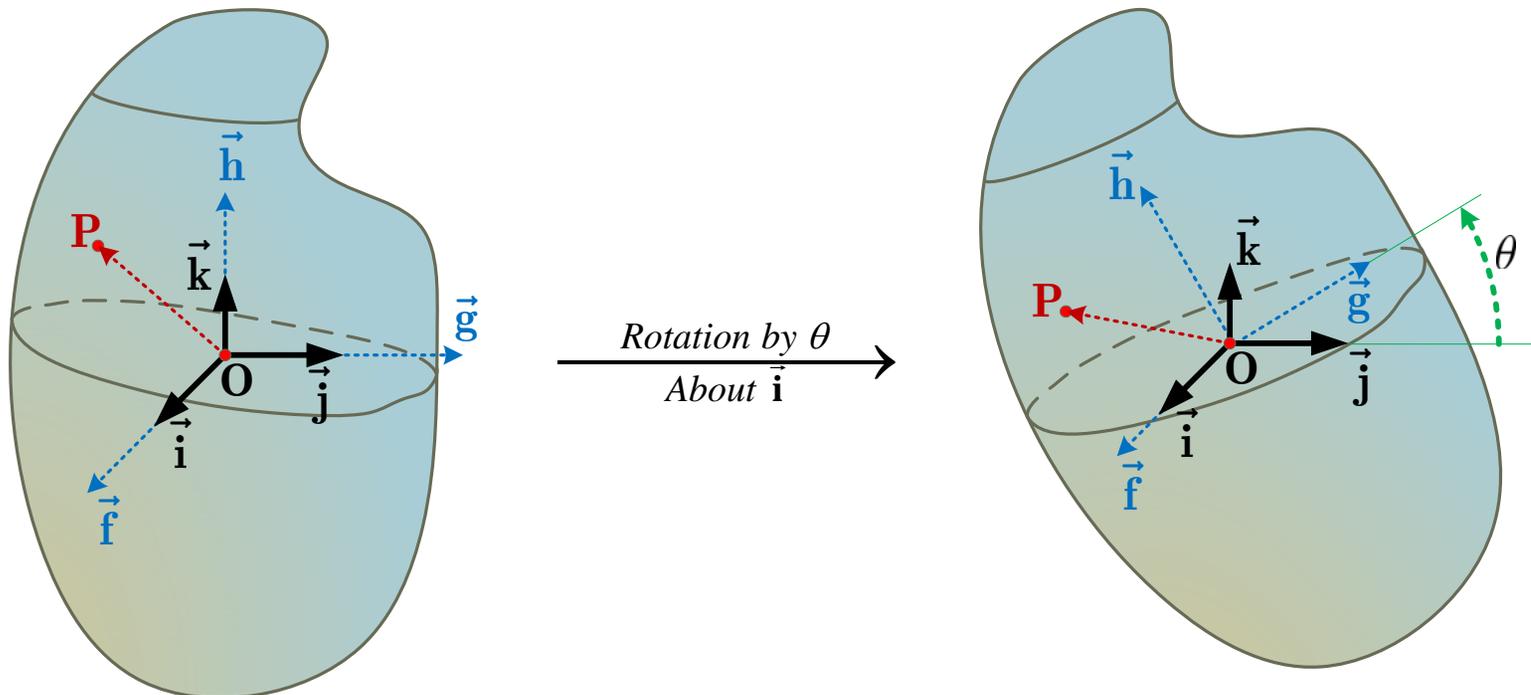
- A rotation matrix is tied to two RFs: a source, and a destination
- It makes sense to expect to see two subscripts attached to  $\mathbf{A}$ : one for the destination RF, one for the source RF
- On the previous slide we used the notation  $\mathbf{A}_i$  for the matrix that gives the transformation from L-RF <sub>$i$</sub>  to the G-RF
- A more consistent notation would have been  $\mathbf{A}_{0i}$ , to indicate that the destination is “0”; i.e., the G-RF, and the source is L-RF <sub>$i$</sub>
- This notation convention; i.e., having two subscripts, would help put things in perspective when we discussed the matrices  $\mathbf{A}_{ij} = \mathbf{A}_i^T \mathbf{A}_j$  on the previous slide: L-RF <sub>$i$</sub>  is the destination, L-RF <sub>$j$</sub>  is the source
- NOTE: Because of convenience, we’ll continue to use  $\mathbf{A}_i$  instead of  $\mathbf{A}_{0i}$



[AO]

## Exercise:

- A body is rotated about the Ox axis by an angle  $\theta$  (see below). What is the expression of the orientation matrix associated with a L-RF attached to the body?
- If the expression of  $\theta(t)$  as a function of time is prescribed, what is the angular velocity of the body in its rotation?

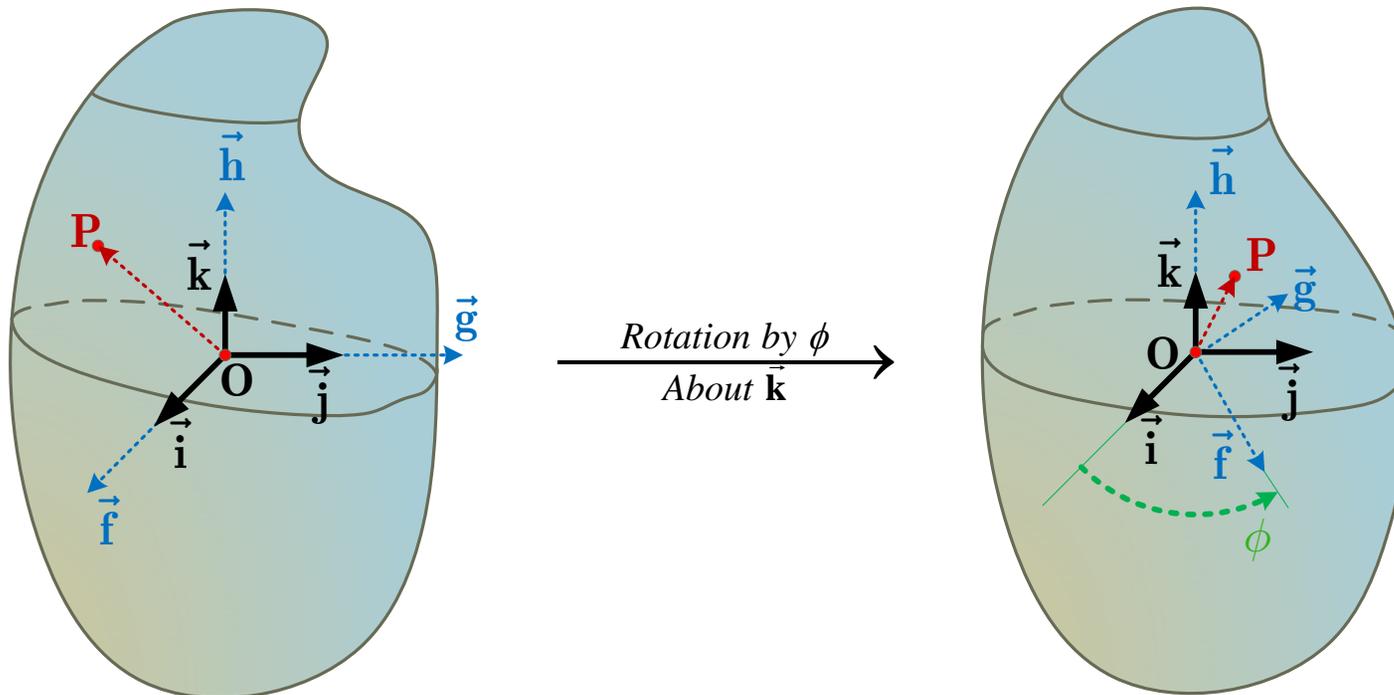




[Homework]

## Exercise:

- A body is rotated about the  $Oz$  axis by an angle  $\phi$ .  
What is the expression of the orientation matrix associated with a L-RF attached to the body?
- If the expression of  $\phi(t)$  as a function of time is prescribed, what is the angular velocity of the body in its rotation?



# Euler Angles

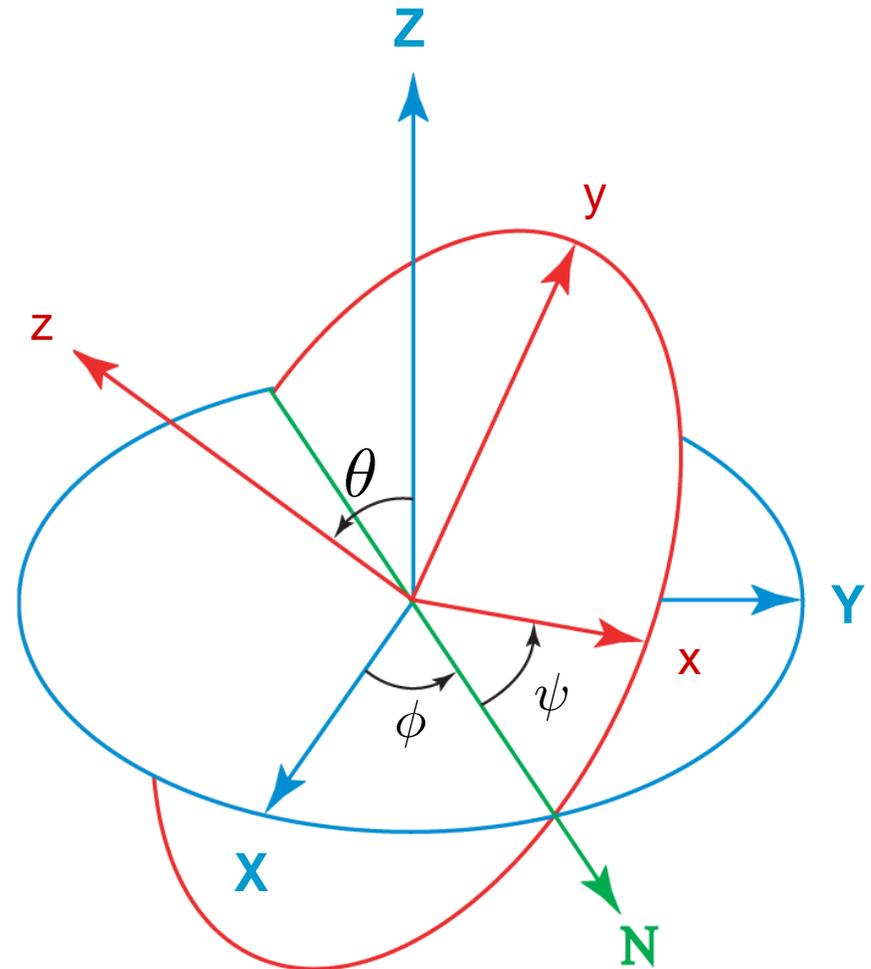
## Putting Things in Perspective, What Comes Next



- We need three generalized coordinates (GCs) to uniquely define the orientation of a body
- We are about to choose the three GCs to be the set of Euler Angles
- When using this set of GCs, we are interested in:
  - Producing the orientation matrix  $\mathbf{A}$  for a given Euler Angles configuration
  - Expressing the connection between the angular velocity of a body and the time derivative of the GCs considered

# Euler Angles

- Euler Angles, definition:
  - A set of three angles used to describe the orientation of a reference frame in 3D space
- Draws on the following observation:
  - You can **align (superimpose) the global reference frame to any arbitrary reference frame** through a sequence of THREE rotation operations
    - Wait till slide 18 to see why the case
- In picture: start from **blue RF**, end in the **red RF** after three rotations
- The sequence of three rotations that we'll consider is
  - About axes Z then X then Z again (called the 3-1-3 sequence)
  - We'll denote the three Euler Angles by  $\psi$ ,  $\phi$ , and  $\theta$ , respectively





# Euler Angles, Quick Remarks

- Some notation conventions:
  - The G-RF is denoted by OXYZ
  - The L-RF that we land on after three  $\sim$ ,  $\prime\prime$ ,  $\prime\prime\prime$  rotations denoted by  $O'x'y'z'$
- Details regarding the three rotations:
  - $O'x'y'z'$  is obtained by rotating  $O''x''y''z''$  around the  $O''z''$  axis by angle  $\sim$
  - $O''x''y''z''$  is obtained by rotating  $O'''x'''y'''z'''$  around the  $O'''x'''$  axis by angle  $\prime\prime$
  - $O'''x'''y'''z'''$  is obtained by rotating OXYZ around OZ axis by angle  $\sim$

# Euler Angles, Quick Remarks [Cntd.]



- There are other Euler Angles choices
  - 1-2-3, 1-3-1, etc.
  - The approach we follow for our 3-1-3 choice to find  $\mathbf{A}$  given the three angles of rotation applies exactly to any other choice of rotation sequence
  - NOTE: ADAMS, a widely used MBD package, uses the 3-1-3 sequence
- Remember that the last two rotations ( $\theta$  and  $\psi$ ) are measured with respect to rotated reference frames
  - $\theta$  about the X axis of  $O''x''y''z''$  to get  $O'x'y'z'$
  - $\psi$  about the Z axis of  $O'x'y'z'$  to get  $Ox'y'z'$

# Expressing $\mathbf{A}$ using Euler Angles (Part 1 of 3)



- Recall that I have a 3-1-3 rotation sequence.
- The last sequence, is a rotation of angle  $\psi$  about  $z''$  to get  $O'x'y'z'$ .
- Therefore, the rotation matrix that relates  $O'x'y'z'$  to  $O''x''y''z''$  is

$$\mathbf{A}_3 = \begin{bmatrix} \cos \psi & -\sin \psi & 0 \\ \sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

- In other words, if I have a vector represented as  $\mathbf{a}'$  in  $O'x'y'z'$ , it will be represented in  $O''x''y''z''$  as

$$\mathbf{a}'' = \mathbf{A}_3 \mathbf{a}'$$

# Expressing A using Euler Angles (Part 2 of 3)



- Just dealt with the last “3” in the 3-1-3 rotation sequence (angle  $\psi$ )
- Focus next on the “1” rotation in the 3-1-3 rotation sequence
  - This is the rotation of angle  $\theta$
- The rotation of angle  $\theta$  about the axis  $O'''x'''$ , takes  $O'''x'''y'''z'''$  into  $O''x''y''z''$

$$\mathbf{A}_2 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix}$$

- In other words, if I have a vector represented in  $O''x''y''z''$  as  $\mathbf{a}''$ , the same vector will be represented in  $O'''x'''y'''z'''$  as

$$\mathbf{a}''' = \mathbf{A}_2 \mathbf{a}''$$

# Expressing A using Euler Angles (Part 3 of 3)



- Just dealt with the “1” in the 3-1-3 rotation sequence (angle  $\psi$ )
- Focus next on the first “3” rotation in the 3-1-3 rotation sequence
  - This is the rotation of angle  $\phi$
- The rotation of angle  $\phi$  about the axis OX, takes OXYZ into O''x''y''z''

$$\mathbf{A}_1 = \begin{bmatrix} \cos \phi & -\sin \phi & 0 \\ \sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

- In other words, if I have a vector represented in O''x''y''z'' as  $\mathbf{a}''$ , the same vector will be represented in OXYZ as

$$\mathbf{a} = \mathbf{A}_1 \mathbf{a}''$$

# Expressing A using Euler Angles

## ~ Putting it All Together ~

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- A Z-X-Z (or 3-1-3) rotation sequence takes OXYZ to O`x`y`z`

- Recall that

- Given  $\mathbf{a}'$ , you get  $\mathbf{a}''$  as

$$\mathbf{a}'' = \mathbf{A}_3 \mathbf{a}'$$

- Given  $\mathbf{a}''$  you get  $\mathbf{a}'''$  as

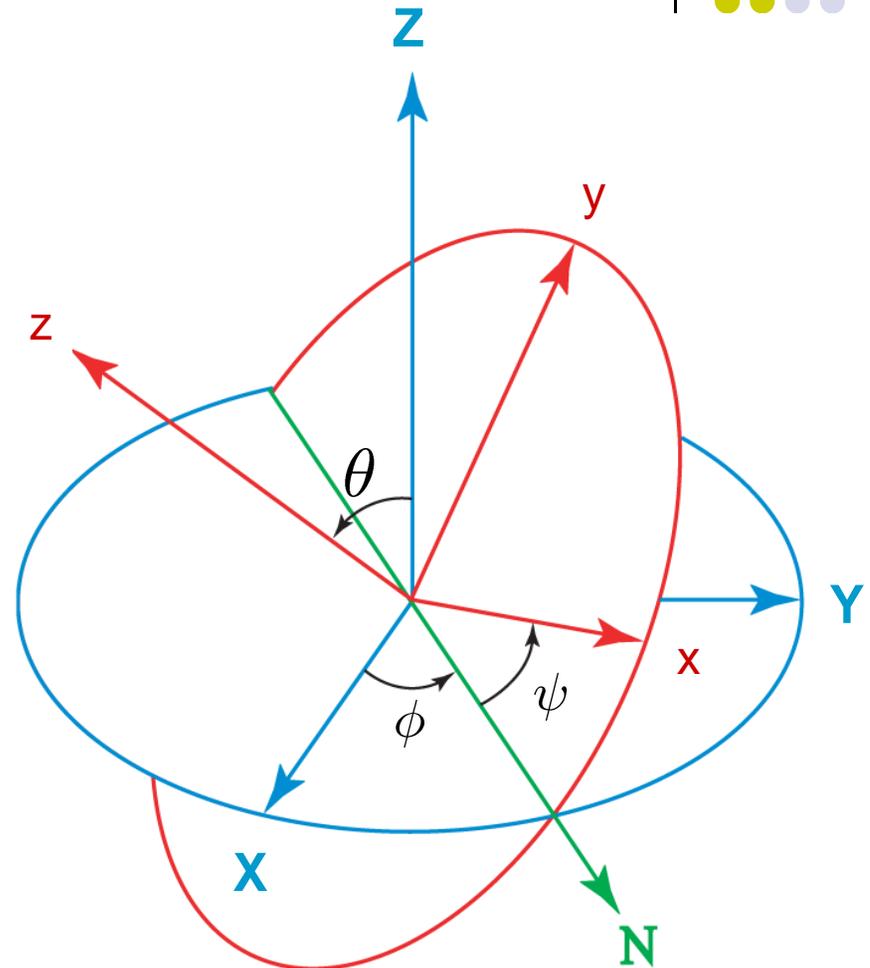
$$\mathbf{a}''' = \mathbf{A}_2 \mathbf{a}''$$

- Given  $\mathbf{a}'''$  you get  $\mathbf{a}$  as

$$\mathbf{a} = \mathbf{A}_1 \mathbf{a}'''$$

- Therefore,

$$\mathbf{a} = \mathbf{A}_1 \mathbf{a}''' = \mathbf{A}_1 (\mathbf{A}_2 \mathbf{a}'') = \mathbf{A}_1 (\mathbf{A}_2 (\mathbf{A}_3 \mathbf{a}')) = \mathbf{A}_1 \mathbf{A}_2 \mathbf{A}_3 \mathbf{a}' \Rightarrow \mathbf{A} = \mathbf{A}_1 \mathbf{A}_2 \mathbf{A}_3$$



# Expressing $\mathbf{A}$ using Euler Angles

## ~ Putting it All Together ~



- Using the expression of the matrices  $\mathbf{A}_1$ ,  $\mathbf{A}_2$ ,  $\mathbf{A}_3$ , one gets for the expression of the orientation matrix  $\mathbf{A}$

$$\mathbf{A} = \mathbf{A}_1 \mathbf{A}_2 \mathbf{A}_3 = \begin{bmatrix} \cos \phi & -\sin \phi & 0 \\ \sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} \cos \psi & -\sin \psi & 0 \\ \sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

- Carrying out the above multiplications we get

$$\mathbf{A} = \begin{bmatrix} \cos \psi \cos \phi - \cos \theta \sin \phi \sin \psi & -\sin \psi \cos \phi - \cos \theta \sin \phi \cos \psi & \sin \theta \sin \phi \\ \cos \psi \sin \phi + \cos \theta \cos \phi \sin \psi & -\sin \psi \sin \phi + \cos \theta \cos \phi \cos \psi & -\sin \theta \cos \phi \\ \sin \theta \sin \psi & \sin \theta \cos \psi & \cos \theta \end{bmatrix}$$

- [Homework]: Provide two proofs that  $\mathbf{A}^T \mathbf{A} = \mathbf{A} \mathbf{A}^T = \mathbf{I}$

# Expressing A using Euler Angles

## ~ Two Questions ~



- Some questions that ought to be asked
  1. Should the order (sequence)  $\sim$   $\$$  „# $\$$  " be observed?
  2. You can always find one set of  $\sim$ , „, " angles to bring G-RF into L-RF
    - Is this set unique?
    - If not, do you run into any issue when you have more 3-1-3 rotations that relate the G-RF and the L-RF?

# Expressing A using Euler Angles

## ~ Two Answers ~



- Answers to previous two questions:
  1. The order of the rotation should be observed since it's important. If you change the order this will land you in a completely different rotational configuration
  2. The only time when you run into a problem is when  $\alpha = k\pi$  (the "1" rotation in the 3-1-3 sequence is any integer multiple of  $\pi$ ).
    - In this case it's not clear how to split the rotations about the Z axes (the first "3" and the last "3" in the 3-1-3 sequence)
    - In this case you cannot rely on this set of generalized coordinates since there is a loss of uniqueness associated with them



[AO]

## Exercise

- The purpose of this exercise is to demonstrate that there is no **global** one-to-one mapping between the nine direction cosines of **A** and the three generalized coordinates  $\psi, \theta, \phi$  used to describe the orientation of a L-RF:
  - Take  $\phi=20, \theta=0$ , and  $\psi=60$ . Compute **A**
  - Take  $\phi=40, \theta=0$ , and  $\psi=40$ . Compute **A**
  - Both cases lead to the same **A**
    - This is called the singularity associated with the Euler angles, and it is unavoidable
    - A solution is to start using a different L-RF<sub>new</sub> when the initial L-RF is associated with a value of  $\psi \sim k\pi$ , where k is any integer
      - This is possible since a L-RF is just an accessory for you to characterize the attitude (orientation) of a rigid body
  - NOTE: People have been attempting to use different generalized coordinates to determine in a more robust fashion the orientation of a body with respect to a global reference frame

# Quick Remark



- The fact that a set of three GCs cannot be found to express **\*globally\*** the orientation of a body with respect to the G-RF proved in 1964:
  - Stuelpnagel, J., “On the parametrization of the three-dimensional rotation group”, SIAM Review, 1964. 6: p. 422-430.
  - Paper available on the class website
- Note that this does not mean that you cannot express **A** as a function of three GCs **\*locally\***
  - This is in fact guaranteed by last lecture’s proof that drew on the Implicit Function Theorem



## **Expressing the Angular Velocity when Using Euler Angles**

# Quick Review, Angular Velocity



- Note that since  $\mathbf{A}$  is orthonormal,

$$\mathbf{A}\mathbf{A}^T = \mathbf{A}^T\mathbf{A} = \mathbf{I}$$

- Take a time derivative to eventually get

$$\dot{\mathbf{A}}\mathbf{A}^T = -\mathbf{A}\dot{\mathbf{A}}^T = -\left(\dot{\mathbf{A}}\mathbf{A}^T\right)^T$$

Identity matrix

- This means that the matrix product at the left is a skew-symmetric matrix
  - Therefore there is a generator vector  $\omega$  that can be used to represent this skew-symmetric matrix:

$$\dot{\mathbf{A}}\mathbf{A}^T = \tilde{\omega}$$

- By definition, the generator vector  $\omega$  is called the angular velocity of the body on which the L-RF is attached**
- NOTE:  $\omega$  is an attribute of the body, and not of the L-RF attached to it**

# Angular Velocity for 3-1-3 Euler Sequence



- When using the 3-1-3 Euler angles, based on the expression of  $\mathbf{A}$ , one gets:

$$\tilde{\omega} = \dot{\mathbf{A}}\mathbf{A}^T = (\dot{\mathbf{A}}_1\mathbf{A}_2\mathbf{A}_3 + \mathbf{A}_1\dot{\mathbf{A}}_2\mathbf{A}_3 + \mathbf{A}_1\mathbf{A}_2\dot{\mathbf{A}}_3)\mathbf{A}_3^T\mathbf{A}_2^T\mathbf{A}_1^T$$

- What you additionally know is that:

$$\dot{\mathbf{A}}_1 = \dot{\phi} \begin{bmatrix} -\sin \phi & -\cos \phi & 0 \\ \cos \phi & -\sin \phi & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\dot{\mathbf{A}}_2 = \dot{\theta} \begin{bmatrix} 0 & 0 & 0 \\ 0 & -\sin \theta & -\cos \theta \\ 0 & \cos \theta & -\sin \theta \end{bmatrix}$$

$$\dot{\mathbf{A}}_3 = \dot{\psi} \begin{bmatrix} -\sin \psi & -\cos \psi & 0 \\ \cos \psi & -\sin \psi & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

# Angular Velocity for 3-1-3 Euler Sequence



- If you carry out the horrific matrix multiplications you end up with the following expression for  $\omega$ :

$$\omega = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \dot{\phi} + \begin{bmatrix} \cos \phi \\ \sin \phi \\ 0 \end{bmatrix} \dot{\theta} + \begin{bmatrix} \sin \theta \sin \phi \\ -\sin \theta \cos \phi \\ \cos \theta \end{bmatrix} \dot{\psi}$$

- Equivalently, you can write this in matrix form like

$$\omega = \begin{bmatrix} 0 & \cos \phi & \sin \theta \sin \phi \\ 0 & \sin \phi & -\sin \theta \cos \phi \\ 1 & 0 & \cos \theta \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} \equiv \mathbf{B}\dot{\epsilon}$$

...where the array of generalized coordinates  $\epsilon$  is defined as

$$\epsilon = \begin{bmatrix} \phi \\ \theta \\ \psi \end{bmatrix}$$

# Angular Velocity for 3-1-3 Euler Sequence



- There is a simpler way to get  $\tilde{\omega}$  though, and it draws on the following identity that we proved last time:

$$\widetilde{(\mathbf{A}\bar{\mathbf{s}})} = \mathbf{A}\tilde{\mathbf{s}}\mathbf{A}^T$$

- The above identity is used in conjunction with :

$$\tilde{\omega} = \dot{\mathbf{A}}\mathbf{A}^T = (\dot{\mathbf{A}}_1\mathbf{A}_2\mathbf{A}_3 + \mathbf{A}_1\dot{\mathbf{A}}_2\mathbf{A}_3 + \mathbf{A}_1\mathbf{A}_2\dot{\mathbf{A}}_3)\mathbf{A}_3^T\mathbf{A}_2^T\mathbf{A}_1^T$$

- Open up the parenthesis above to get that

$$\omega = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \dot{\phi} + \begin{bmatrix} \cos \phi \\ \sin \phi \\ 0 \end{bmatrix} \dot{\theta} + \begin{bmatrix} \sin \theta \sin \phi \\ -\sin \theta \cos \phi \\ \cos \theta \end{bmatrix} \dot{\psi}$$

# Angular Velocity for 3-1-3 Euler Sequence



- The previous slide says that you can compute the time derivatives of the Euler angles given  $\omega$  by solving the linear system

$$\mathbf{B}\dot{\epsilon} = \omega$$

- Note that  $\det(\mathbf{B}) = \sin\theta$ , which yet again indicates that when the second rotation (the “1” in the 3-1-3 sequence) is  $\theta = k\pi$ , the matrix  $\mathbf{B}$  is singular and you are in trouble (singular configuration)
- To avoid this situation people introduced a set of four “Euler parameters” which have less issues albeit at a slight increase in abstraction
  - You have some redundancy in information (three parameters are necessary, yet you have four Euler parameters, which leads to one additional constraint equation)